



## Abstract

This paper introduces a Fractal Patch Antenna (FPA) integrated with Photonic Crystals (PhC) designed for Intelligent Transportation Systems (ITS) in the Millimeter-wave bands (mmWaves) given the importance of the application of mmWaves in Vehicle-to-Everything (V2X) networks, we assumed, as examples, that the antenna is designed to resonate at three frequency bands: 31.42 GHz, 37.76 GHz, and 38.92 GHz. With a gain of 10.88 dBi, at 38.92GHz, the antenna demonstrates promising signal reception and transmission capabilities, which are anticipated to be important for ITS operations. The antenna bandwidth covers multiple frequency bands, enabling versatile communication in mmWaves V2X applications. To evaluate the performance of the antenna, we conducted a detailed analysis of its configuration. This included a comparison of the antenna with and without the PhC integration, as well as an exploration of rectangular lattice structure. In addition, variations in hole sizes and spacing were examined to assess their impact on key parameters such as the gain and reflection coefficient. The integration of fractal geometry and PhC structures results in a compact, high-performance antenna suitable for mmWave communication. The integration of fractal geometry and PhC structure results in compactness and high performance in mmWaves communication applications. Through simulation and analysis, including radiation pattern, gain, and reflection coefficient plot assessment, the antenna performance is thoroughly evaluated. The study highlights the potential of the proposed FPA-PhC antenna configuration to enhance communication networks within the ITS, significantly advancing the ITS system with support from the mmWave bands.

## Plain Language Summary

This study introduces a Fractal Patch Antenna (FPA) integrated with Photonic Crystals (PhC) to improve communication within Intelligent Transportation Systems (ITS) by leveraging millimeter-wave (mmWave) bands. The antenna is designed to operate efficiently at frequencies of 31.42 GHz, 37.76 GHz, and 38.92 GHz, achieving a high gain of 10.88 dBi at 38.92 GHz, which improves its ability to send and receive signals. With a broad bandwidth covering multiple frequencies, it supports versatile applications, particularly in Vehicle-to-Everything communication. We have conducted a comparative analysis between the FPA with and without the PhC, as well as variations in rectangular lattice configurations and changes in hole sizes and spacing. The use of fractal geometry and PhC with square lattice ensures compactness while significantly improving performance. Comprehensive simulations and analyses of key parameters such as radiation patterns, gain, and reflection coefficients validate the antenna's capability, demonstrating its potential to advance ITS communication networks and enable efficient mmWave communications.

## 1 INTRODUCTION

Every year, millions of road accidents could be prevented with advanced vehicle communication systems. Vehicle-to-Everything (V2X) technology, particularly using millimeter-wave (mmWave) bands, promises to transform road safety with higher data rates. This highlights the importance of developing antennas that operate efficiently at high frequencies, enabling high-speed communication between vehicles and the infrastructure. mmWave frequencies are

69 particularly suited for short-range, high-data-rate applications in dense ur-  
70 ban environments where infrastructure can support the deployment of small  
71 cells and repeaters. These antennas are essential for leveraging the high data  
72 rates and low latency offered by the mmWave bands, facilitating advanced  
73 V2X communication systems. A Fractal Patch Antenna (FPA) based on Pho-  
74 tonic Crystals (PhC) is a type of antenna that utilizes fractal geometry and  
75 PhC to achieve enhanced performance compared to traditional patch anten-  
76 nas. Howell (Howell, 1975) first introduced the microstrip antenna in 1972,  
77 with the patch antenna representing a variant of the compact antenna design.  
78 Patch antennas can take various forms, including circular, rectangular, tri-  
79 angular, and square shapes, with different feeding methods available. While  
80 patch antennas offer advantages such as lightweight construction, minimal man-  
81 ufacturing costs, operation at microwave frequencies, compatibility with in-  
82 tegrated circuit technology, and compactness, they suffer from poor gain. This  
83 paper is organized to systematically explore and compare antenna configu-  
84 rations for improved V2X communication. Not only does one delve into the  
85 design and analysis of antennas with square lattice photonic crystals, but one  
86 also discusses the antenna design without PhC integration. Antennas with  
87 square lattice photonic crystals are then compared with rectangular lattice  
88 designs, highlighting differences in gain and bandwidth performance. The ef-  
89 fects of varying the size and spacing of PhC on the antenna’s performance are  
90 explored as well, providing insights into the tunability and adaptability of these  
91 configurations in practical deployments.

## 92 1.1 Background

93 Various scenarios have been proposed to achieve the required high gain  
94 and high bandwidth by including the utilization of metamaterials as substrates  
95 (Soily et al., 2022; Hamza et al., 2022; K & Pradeep, 2022; Sinha et al., 2021;  
96 Deshmukh et al., 2019, 2019), parasitic patches (Awan et al., 2021; Sharma  
97 et al., 2021; El Arrouch et al., 2022; Erbaş, 2020; Oliveira et al., 2021; Hos-  
98 sain et al., 2021; Asok & Dey, 2021), air gaps (Tanveer et al., 2021), slots (J. Zhang  
99 & Mao, 2020; Khabba et al., 2022; Mangal & Gour, 2021; Lin & Omote, 2021;  
100 Olawoye & Kumar, 2020; Hao et al., 2020; C. Chen, 2022), shorting pins (Yang  
101 et al., 2021; Fang et al., 2022; Gautam & Kumar, 2023; Wu et al., 2023; Ah-  
102 mad et al., 2020, 2020; X. Zhang et al., 2021), metamaterials (Sufian et al.,  
103 2021; Kulkarni & Deshpande, 2024; Mishra et al., 2023; Bakir & Sahin, 2023;  
104 Yin et al., 2023; Kumar et al., 2023), dielectric substrates (Dong et al., 2022;  
105 Desai & Bindu, 2023; Jiang et al., 2023; Li et al., 2023; Muangrung et al., 2023),  
106 antenna array (Yan et al., 2024), configurations, multilayered substrate tech-  
107 niques (Zhao et al., 2023), and incomplete grounds (Biswas et al., 2023). Fur-  
108 thermore, the use of PhC structures has been proposed to address surface waves  
109 (Messatfa et al., 2022; Benlakehal et al., 2024, 2023, 2022; Saurabh & Meshram,  
110 2022; Temmar et al., 2023). PhC, periodic dielectric structures, prohibit elec-  
111 tromagnetic waves of specific directions from passing through them (Messatfa  
112 et al., 2022; Salehi et al., 2020). Beyond 5G and 6G networks promise trans-  
113 formative capabilities, including high data rates, low latency, and massive con-  
114 nectivity, making them well-suited for enhancing Intelligent Transportation  
115 Systems (ITS) functionalities. The design of the antenna presented uses the  
116 concept of fractal geometry, which involves repeating patterns at different scales.  
117 Incorporating fractal elements into the patch structure enables us to achieve  
118 a more compact antenna size without destroying performance. Miniaturiza-  
119 tion is crucial for the integration of the antenna into small, space-constrained  
120 devices commonly found in ITS. A key aspect of antenna design is the use

121 of a PhC as a substrate material. PhC are materials that show unique elec-  
122 tromagnetic properties, including control over the propagation of waves.

## 123 **1.2 The True Reasons for Designing V2X Antennas in the Mil-** 124 **limeter Wave Bands**

125 Advances in wireless communications, particularly intelligent vehicular  
126 communications, require frequency spectrum allocation and management strate-  
127 gies that accommodate the increasing demand for bandwidth, efficiently uti-  
128 lize it, and mitigate interference.

129 The functionality of Autonomous and Connected Vehicles (ACVs) re-  
130 lies on data from various sensors, necessitating high communication bandwidths,  
131 often in the gigabits-per-second range. mmWave technology is crucial for achiev-  
132 ing this, enabling high-performance Vehicle-to-Vehicle (V2V), Vehicle-to-Infrastructure  
133 (V2I), and intra-vehicular communications. mmWave V2V links allow vehi-  
134 cles to share raw data with neighboring vehicles, enhancing situational aware-  
135 ness. V2I links use mmWave to improve road safety applications by trans-  
136 mitting vehicle data to cloud resources for processing. mmWave links with  
137 high data rate are also used to download real-time maps and dynamic envi-  
138 ronment information (Hakak et al., 2023). ACVs utilize various mmWave com-  
139 munication bands, including 5G bands like 28 GHz, unlicensed bands like 60  
140 GHz, and automotive radar bands like 24 GHz and 76 GHz (Ahangar et al.,  
141 2021). However, designing 5G antennas for autonomous vehicles poses sig-  
142 nificant challenges (Saad et al., 2023), as these antennas must provide reli-  
143 able communication with a wide radiation pattern and a wide operating fre-  
144 quency range.

145 The author in (Mukherjee, Roy, & Mukhopadhyay, 2022) presents a SISO  
146 antenna in Y shape designed to cover the (26.5 - 28) GHz, 5G mmWave bands.  
147 This paper also provides a comparison between the proposed SISO antenna  
148 and current MIMO antennas used in automotive applications. Traditionally,  
149 licensed sub-6 GHz bands such as 2.4 GHz and 5.9 GHz have been commonly  
150 used for ITS (Soto et al., 2022). However, the emerging 26.5 GHz and 28 GHz  
151 mmWave 5G bands (Mukherjee, Mukhopadhyay, & Roy, 2022) are being ex-  
152 plored for ITS due to their potential to enable much faster data rates and lower  
153 latency compared to sub-6 GHz bands (Mukherjee et al., 2020). This capa-  
154 bility is crucial for V2V communication, which is essential for automated driv-  
155 ing, optimizing fuel efficiency, and providing rapid communication to prevent  
156 breakdowns. In (Niranjan Prasad et al., 2023), the design and analysis of a  
157 wideband 5G antenna for autonomous vehicles is discussed. The proposed an-  
158 tenna utilizes Tesla geometry, which is known for its high gain and wide-angle  
159 radiation pattern. The results show a gain of 4.5 dB, a bandwidth of 2.442  
160 GHz, and an operational frequency of 29.2 GHz. In (Saad et al., 2023), the  
161 design of NR V2X SL communication prioritizes the FR2 (24.25 – 52) GHz  
162 band to support high data rates (50-1000) Mb/s. Beamforming is essential  
163 to counteract pathloss at higher frequencies and can also be used for FR1.  
164 It enables directional transmission, facilitates spatial reuse of resources in con-  
165 gested areas, and expands the coverage of the V2X network. Additionally, beam-  
166 forming allows controlled sidelink power.

167 The mmWaves offer the potential for achieving ultra-high data rates,  
168 which are essential for supporting these advanced applications. With limited  
169 available spectrum below 6 GHz, it is challenging to meet the required data  
170 rates for advanced V2X applications. The mmWaves provide a large trans-  
171 mission bandwidth, which can help address the scarcity of spectrum and sup-

172 port the high data rate demand of V2X communications. Despite the chal-  
173 lenges posed by high atmospheric attenuation and significant path loss in the  
174 mmWaves channel, specific beamforming can mitigate these issues by con-  
175 centrating the transmitted signal in one direction (D. Zhang et al., 2018).

176 As a fundamental aspect of ITS, the utilization of beyond 5G (B5G) tech-  
177 nology in V2X communication has garnered global attention. This cutting-  
178 edge technology promises to revolutionize the way vehicles interact with each  
179 other (V2V) and with infrastructure (V2I), improving safety on roads (Ye et  
180 al., 2024).

181 The 3rd Generation Partnership Project (3GPP) has acknowledged the  
182 performance challenges inherent in V2X communication and addressed them  
183 in its Release 17. This release standard stipulates that the 5G new radio (NR)  
184 frequency range 2 (FR2), spanning from 24 GHz to 71 GHz, can be employed  
185 for V2X communication. However, several challenges arise when operating  
186 in this high-frequency band.

187 The advent of 5G NR technology has brought about significant advance-  
188 ments in vehicular communication, particularly in the context of V2X net-  
189 works (Gyawali et al., 2021). V2X networks encompass various types of com-  
190 munication between vehicles, infrastructure, pedestrians, and other entities,  
191 enabling better road safety and enhanced driving experiences (Garcia et al.,  
192 2021). One key aspect of 5G NR-based V2X communication is its use of high  
193 communication frequencies in the FR2 spectrum, which offers increased spec-  
194 trum resources in V2I communication scenarios (Saad et al., 2021). In the 3GPP  
195 Release 17 standard, the upper bound of the FR2 spectrum has been extended  
196 to 71GHz. As a result, high-frequency wireless communication can be expected  
197 to play a significant role in future B5G V2X networks (3GPP, 2021; 3rd Gen-  
198 eration Partnership Project (3GPP), 2023). In summary, while there are chal-  
199 lenges to overcome, mmWaves with ongoing research and development efforts  
200 focused on enabling technologies, mmWaves NR-V2X could indeed be a suit-  
201 able option to enhance V2X communication capabilities (S. Chen et al., 2024;  
202 Saad et al., 2023). Sidelink communications, in the context of wireless net-  
203 working, refer to a mode of direct communication between devices without  
204 the need for intermediation by a central network infrastructure. It allows de-  
205 vices to establish peer-to-peer connections, enabling efficient data exchange  
206 and collaboration, particularly in scenarios where direct communication is ben-  
207 efiticial, such as V2V communication in ITS or device-to-device (D2D) com-  
208 munication in crowded urban environments. Some argue that there is not enough  
209 spectrum in the Intelligent Transportation System (ITS) band to meet the  
210 needs of V2X communications. One way to address this problem is to make  
211 the spectrum available somewhere in the FR2 bands. That is the approach  
212 taken in this paper. Another way to address that problem is to give V2X de-  
213 vices access to bands that are currently unlicensed as proposed in (Peha, 2023;  
214 Peha et al., 2024), because sharing between V2X devices and unlicensed de-  
215 vices can be very efficient (Ligo & Peha, 2019). The 3GPP Release 17 & 18  
216 for the next generation of V2X will support operations in the FR2 spectrum  
217 range, which is from 24.25 GHz to 71 GHz (Saad et al., 2023), and researchers  
218 have been exploring the use of mmwave spectrum for V2X. It is not yet known  
219 which spectrum band at these higher frequencies will be used. The October  
220 2024 V2X interoperability demonstration in Cheyenne, Wyoming, revealed  
221 that some participants were exploring the use of complementary spectrum be-  
222 yond the 5.9 GHz band, reflecting a growing interest in leveraging alterna-  
223 tive frequency ranges for advanced V2X applications (U.S. Department of Trans-

224 portation ( October), 2024). For this research, as an example, we designed  
225 an antenna that operates at 31.42 GHz, 37.76 GHz, and 38.92 GHz.

### 226 1.3 Proposed Approach

227 The proposed FPA offers significant advantages in facilitating V2I com-  
228 munication. The use of fractal geometry combined with the PhC structure  
229 allows the antenna to operate on a wide range of frequencies, providing in-  
230 creased bandwidth for data transmission. This allows for the transmission of  
231 big data at high data rates, essential for supporting applications such as real-  
232 time video feeds and V2V communications. FPAs are known for their com-  
233 pact and low-profile design, making them ideal for integration into vehicles  
234 without adding significant bulk or altering the vehicle’s aerodynamics.

235 The proposed FPA offers significant advantages for V2I communication.  
236 The combination of fractal geometry and PhC structure enables the antenna  
237 to operate over a wide range of frequencies, increasing bandwidth for data trans-  
238 mission. This capability supports high- data-rate applications such as real-  
239 time video feeds and V2V communications. Known for their compact and low-  
240 profile design, FPAs are ideal for vehicle integration without adding signif-  
241 icant bulk or altering aerodynamics. This versatility allows for seamless in-  
242 tegration with existing communication infrastructures and supports future  
243 advancements in vehicular communication. By integrating the antenna into  
244 vehicles, they can establish reliable and high data-rate links with roadside in-  
245 frastructure such as traffic lights, road signs, and traffic management systems.

246 Additionally, the antenna facilitates communication with toll systems,  
247 parking meters, and charging stations, allowing seamless and efficient services  
248 such as automated toll payments and electric vehicle charging coordination.  
249 In the realm of Vehicle-to-Pedestrian (V2P) communications, the FPA plays  
250 a crucial role in improving road safety. By equipping vehicles with antenna,  
251 they can establish short-range wireless connections with pedestrian devices,  
252 such as smartphones or wearable devices. FPA enables real-time exchange of  
253 information, warnings, and alerts, allowing vehicles to inform pedestrians of  
254 their presence when approaching crosswalks or provide warnings in the event  
255 of potential collisions. This type of communication fosters safer interactions  
256 between vehicles and pedestrians, contributing to overall road safety.

257 Moreover, the FPA facilitates seamless V2V communication, essential  
258 to improve traffic safety and efficiency. Integrating the antenna into vehicles  
259 enables them to establish direct wireless links with nearby vehicles, facilitat-  
260 ing the real-time exchange of information such as vehicle position, speed, and  
261 trajectory. This enables collaborative collision avoidance and cooperative adap-  
262 tive cruise control, among other applications, leading to safer and more ef-  
263 ficient traffic flow.

264 To evaluate the performance of the FPA, extensive simulations are per-  
265 formed using the high-frequency structural simulation instrument HFSS, (Ansys,  
266 2023). The analysis encompassed parameters such as radiation patterns, gain,  
267 and bandwidth. The results obtained from these simulations examine the ex-  
268 ceptional gain characteristics of the proposed antenna in the millimeter-wave  
269 ITS range, which align well with the anticipated requirements for ITS. Rel-  
270 evantly, the importance of the application of mmWaves in V2X networks led  
271 us to assume, as examples, that the antenna resonates at three key frequen-  
272 cies: 31.42 GHz, 37.76 GHz and 38.92 GHz, aligning with the future frequency  
273 spectrum for ITS applications.

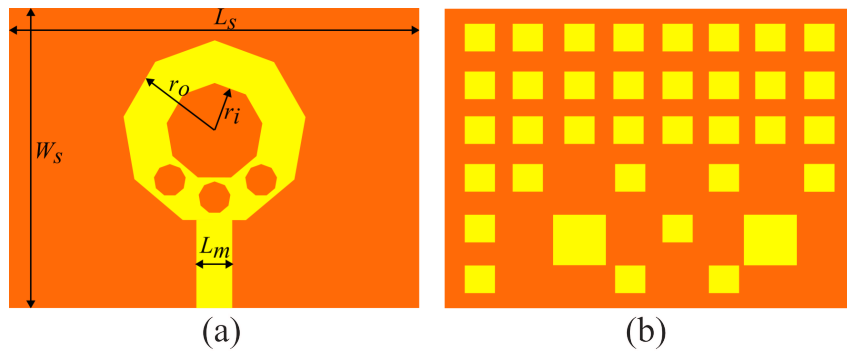
## 1.4 Structure of the Paper

To rest of the paper, organized as follows: Section 2 explores the integration of PhC antennas for augmented performance, with a specific focus on the future potentials and implications of PhC antennas in V2X communications. Section 3 examines the critical aspects of antenna design and performance analysis and includes the analysis of the reflection coefficient (S11) plot for three resonance bands, radiation pattern plot, gain plot and directivity plot along with the 3D radiation pattern. The study includes a detailed comparison of different lattice geometries, such as, square lattices, antenna without PhC, and rectangular lattices whilst evaluating the impact of the hole and space size variations on parameters such as S11 and gain. In Section 4 the antenna is introduced, highlighting its compact design, beyond 5G capabilities, and potential contributions to the advancement of communication technologies and V2V. Finally, Section 5 presents the conclusions and summarizes the findings of the study, offering an overview of the primary contributions and briefly outlining suggestions for future research.

## 2 ANTENNA DESIGN

Antenna design involves engineering the antenna structure and its associated components to enhance its performance for a given application. The appropriate type of antenna (such as a dipole or patch antenna), the size and shape of the antenna, and the materials used to fabricate it are essential considerations. To ensure that the antenna meets the desired specifications in terms of gain, directivity, and radiation pattern, the design process includes simulation and testing. In the study, a copper nonagon is chosen as a radiation patch.

Fig. 1(a) shows the microstrip antenna configuration proposed for the triple band antenna. The antenna design is implemented on a Gallium Arsenide (GaAs) substrate with dimensions  $L_s \times W_s \times h = 4.9 \times 5.9 \times 1 \text{ mm}^3$ ,  $r_o = 0.85 \text{ mm}$ ,  $r_i = 0.5 \text{ mm}$ , and  $L_m = 0.7 \text{ mm}$  and  $\epsilon_r = 12.9$ .



**Figure 1.** (a) Configuration of the proposed microstrip patch antenna, illustrating its dimensions and layout fig.a.

(b) Structure of the square lattice photonic crystal used for the ground and substrate of the antenna fig.b.

The shape of the antenna is a regular nonagon made of copper, with three nonagonal fractals created in it, the thickness of the copper patch is 0.035 mm, it is fed by a  $50 \Omega$  microstrip line, with a strip width of 0.9 mm. The height

306 of the ground copper is 0.035 mm. PhC substrate is created by integrating  
 307 the cuboid in a bed with a diagonal of 0.2 mm and a distance between each  
 308 cuboid of 1 mm. As mentioned earlier, reducing the size of the cuboids and  
 309 increasing the distance between the cylinders will reduce the gain and band-  
 310 width of the antenna.

311 Fig. 1 (b), shows the structure of PhC for the ground and substrate. The  
 312 structure of a PhC consists of a periodic arrangement of dielectric materials  
 313 with alternating high and low refractive indices. Periodicity creates a pho-  
 314 tonic bandgap, a range of frequencies where light propagation is forbidden,  
 315 similar to the bandgap in semiconductors for electrons. These bandgaps are  
 316 crucial for controlling the flow of light, enabling applications such as wave-  
 317 guiding, filtering, and optical sensing. Hence, the introduction of defects within  
 318 the PhC lattice is a key strategy for modifying the optical properties. These  
 319 defect modes act as resonators, prohibiting or guiding light at specific frequen-  
 320 cies, thus enabling functionalities such as efficient light emission, high-Q op-  
 321 tical cavities, and enhanced sensing capabilities.

## 322 2.1 Mathematical Equations

323 To design a patch antenna, it is important to consider several equations.  
 324 The equations considered to calculate the patch length are as follows:

$$L = \frac{c}{2f_0\sqrt{\varepsilon_{eff}}} - 0.824h \left( \frac{(\varepsilon_{eff} + 0.3) \left(\frac{W}{h} + 0.264\right)}{(\varepsilon_{eff} - 0.258) \left(\frac{W}{h} + 0.8\right)} \right) \quad (1)$$

325 where  $L$  is length of the patch,  $c$  is the speed of light,  $W$  is width of the patch,  
 326  $\varepsilon_{eff}$ , is the effective dielectric constant,  $f_0$  is the operating frequency of the  
 327 antenna and  $h$  is the height/thickness of the substrate. The patch width,  $W$ ,  
 328 can be calculated as follows:

$$W = \frac{c}{2f_0\sqrt{\frac{\varepsilon_R + 1}{2}}} \quad (2)$$

329 where  $\varepsilon_R$  is the value of the dielectric constant of the substrate. The effec-  
 330 tive dielectric constant is calculated as follows:

$$\varepsilon_{eff} = \frac{\varepsilon_R + 1}{2} + \frac{\varepsilon_R - 1}{2} \left[ \frac{1}{1 + 12 \left(\frac{W}{h}\right)} \right] \quad (3)$$

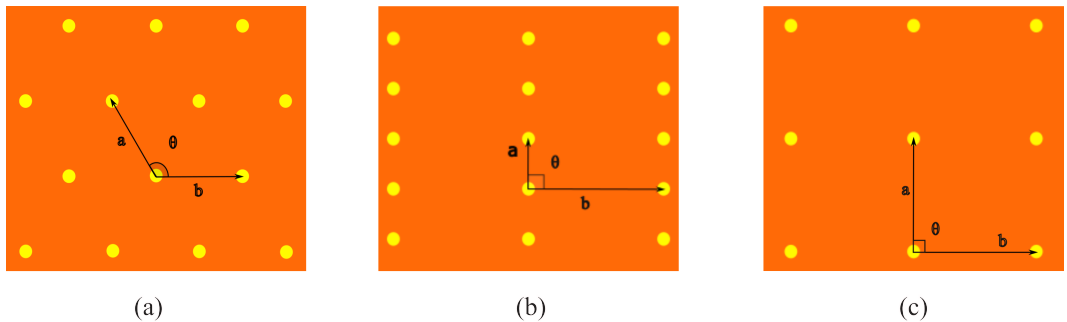
331 For the patch antenna, impedance matching techniques are considered  
 332 to ensure maximum power transfer to the antenna and that the element can  
 333 strongly radiate and contains matching of the input impedance at the end of  
 334 the antenna's feedline (to the feedline's characteristic impedance).

## 335 2.2 Photonic Band Gap Structure

336 A PhC is a periodic structure that exhibits a spatial variation in its di-  
 337 electric properties, causing it to interact with light in unique ways. Much like  
 338 how the arrangement of atoms in a crystal lattice affects the behavior of elec-  
 339 trons in a material, the periodic arrangement of dielectric materials on PhC  
 340 affects the propagation of electromagnetic waves (light) within it. PhC can  
 341 be designed by creating holes or rod shapes in the structure of the antenna  
 342 substrate. By changing the radius and size of the holes or rods shape and chang-  
 343 ing the distance between those, the gain, bandwidth and other features of the  
 344 antenna changes.

345 In two-dimensional PhC design, there are several types of lattices. (hexag-  
 346 onal, square, and rectangular) are considered along with five different shapes  
 347 of scatterers: hexagonal, circle, square, rectangle, and oval. These scatterers  
 348 are considered as dielectric rods in air, or air rods are modeled in dielectric  
 349 media. This choice of configurations underscores the significant effect of lat-  
 350 tice symmetry and scatterer geometry on the size of the PBG. The schematic  
 351 of a photonic crystal lattice in a PhC presented in Fig. 2 offers precise con-  
 352 trol over the propagation of light.

353 A Bravais lattice describes the periodic arrangement of points in space,  
 354 forming the foundation of crystal structures, including applications in pho-  
 355 tonic crystals. In two dimensions, common types of structures include square,  
 356 hexagonal, and rectangular lattices. These structures define how electromag-  
 357 netic waves interact with the material and directly influence the propagation  
 358 of the waves. In square lattices, antenna elements are arranged symmetrically  
 359 and periodically, leading to a uniform and predictable radiation pattern. The  
 360 square lattice simplifies the design and implementation of antenna arrays, ul-  
 361 timately justifying this adoption for systems that require simple and stable  
 362 radiation patterns. In phased array antennas, square lattices allow precise beam  
 363 steering and help reduce side lobes. In a square lattice, the elements are equally  
 364 spaced along the  $x$  and  $y$  axes, ensuring a uniform distance in all directions.  
 365 The high symmetry produces a consistent radiation pattern as elements har-  
 366 moniously contribute to the final outcome with similar phases. This arrange-  
 367 ment prevents signal fluctuations and irregularities in different directions. While  
 368 a hexagonal lattice has equal side lengths ( $a = b$ ) with angles between ad-  
 369 jacent vectors of  $120^\circ$ , a rectangular lattice has unequal side lengths ( $a \neq b$ )  
 370 with angles between adjacent vectors of  $90^\circ$ . On the other hand, a square lat-  
 371 tice has equal side lengths ( $a = b$ ) with angles between adjacent vectors of  
 372  $90^\circ$ , and is often preferred in antenna application, mainly due to its simplic-  
 373 ity, uniform spacing, and symmetrical properties.



**Figure 2.** The three fundamental two-dimensional Bravais lattices: (a) Hexagonal lattice:  $|a| = |b|, \theta = 120^\circ$ ; (b) Rectangular lattice:  $|a| \neq |b|, \theta = 90^\circ$ ; (c) Square lattice:  $|a| = |b|, \theta = 90^\circ$ .

374 Defects in this lattice structure enhance functionality, tunability, sens-  
 375 ing capabilities, and fault tolerance. They enable tailored optical or frequency  
 376 responses, tunable properties, sensing of environmental changes. Inclusion of  
 377 defects expands the application in photonics and optical communication sys-  
 378 tems. A square-shaped PhC has been utilized for the design of the proposed  
 379 antenna. These shapes can provide additional degrees of freedom in tuning  
 380 the PBG compared to other structures. For example, square lattices can ex-  
 381 hibit different symmetry properties and may support different types of pho-  
 382 tonic band gap compared to other lattices. Fig. 2 schematic representations

383 of different PhC lattice configurations provide insight into their structural di-  
384 versity.

385 Photonic Band Gap (PBG) materials are periodic and display broad-  
386 band pass and stop band attributes at microwave frequencies. PBG compo-  
387 nents are composed by introducing periodic disturbances such as PhC rods,  
388 cavities, and patterns in waveguides and substrates. As in PhC photon propa-  
389 gation, the electromagnetic waves in a PBG structure are impeded because  
390 of the periodic discontinuity, hence making a slow wave structure. Within the  
391 PBG, the modes of EM wave propagation have field distributions and disper-  
392 sion properties that differ significantly from those in free space. Due to these  
393 unique properties of PBG materials, they have potential applications in an-  
394 tennas, amplifiers, waveguides, and filters, power combining, phased arrays,  
395 EMC measurements, and many microwave devices. Employing this method  
396 improves gain, suppresses surface waves, and increases antenna bandwidth,  
397 while reducing patch loss.

398 In a recent study of ours (Bagheri et al., 2024), the performance of a  
399 similar photonic crystal antenna was analyzed with and without the integra-  
400 tion of the PhC structure. In that study, the results have clearly demonstrated  
401 the significant enhancements in gain and bandwidth achieved by incorporat-  
402 ing the PhC substrate compared to that achieved by incorporating the con-  
403 ventional configuration. This comparative analysis underscores the effective-  
404 ness of the PhC structure in improving the overall performance of this type  
405 of antennas. Besides, the authors of (Vahdati & Parandin, 2019), have pro-  
406 posed the establishment of a photonic crystal surface that enables antennas  
407 to achieve uniform electromagnetic radiation. Adjusting the underlying mi-  
408 crostrip layer beneath the crystalline layer has shown to expand the band-  
409 width in the 30-80 GHz range by as much as approximately 50 GHz. Further-  
410 more, the antenna gain has improved from 6.45 dB to 7.7 dB, reflecting an  
411 increase of about 1.2 dB. These improvements clearly show that incorporat-  
412 ing the crystal layer leads to a significant enhancement of the bandwidth and  
413 gain of the antennas, particularly when operating at terahertz frequencies.

414 GaAs was selected as the primary material for the proposed antenna sub-  
415 strate due to its customized properties. GaAs acts as a semiconductor with  
416 distinct advantages: it offers superior electron mobility crucial for effective  
417 operation at high frequencies, a wide bandgap essential for achieving high-  
418 speed data transmission, and a lower noise figure resulting in improved sig-  
419 nal clarity.

420 Furthermore, GaAs demonstrates a higher breakdown voltage, enhanc-  
421 ing antenna durability, maintains consistent electrical properties across a broad  
422 range of temperatures, providing reliable performance, and features a low-loss  
423 tangent, minimizing energy loss. GaAs possesses relatively high thermal con-  
424 ductivity, facilitating efficient heat dissipation, thus maintaining antenna per-  
425 formance over extended periods.

426 In the proposed design, we introduce square holes in the GaAs substrate,  
427 beneath the FPA, to create a PhC structure. This modification offers several  
428 benefits. The periodic arrangement of square holes forms a PBG, this allows  
429 precise control over transmission and reflection, enhancing antenna perfor-  
430 mance. The PhC structure influences radiation patterns, enabling directional  
431 beams or beam steering. Modifying the size and arrangement of holes cus-  
432 tomizes the radiation properties for specific applications. The structure con-  
433 fines electromagnetic energy within the antenna, minimizing substrate losses  
434 and enhancing radiation efficiency. Adjusting hole size and spacing tunes PBG

435 and dispersion characteristics, improving antenna performance for the desired  
436 parameters.

437 The defect design offers precise control over the band gap properties of  
438 PhC substrates, enhancing the antenna’s performance and versatility. By strate-  
439 gically designing defects, the band-gap characteristics can be tailored to spe-  
440 cific frequency ranges, improving frequency selectivity and spectral efficiency.  
441 These defects induce localized resonant modes within the band gap, which  
442 can be finely tuned to adjust the antenna’s operating frequency or bandwidth.

443 According to (Roslan et al., 2018), the performance of photonic crys-  
444 tal cavity (PCC) antennas, including resonant frequency, S parameters, gain,  
445 and radiation pattern, is highly sensitive to variations in hole size and spac-  
446 ing. A radius of 9.6  $\mu\text{m}$  resulted in a return loss of -71.94 dB and a gain of  
447 9.730 dB, while a spacing of 100.1  $\mu\text{m}$  achieved a return loss of -56.56 dB and  
448 a gain of 9.726 dB. These findings demonstrate that precise geometric adjust-  
449 ments are essential for effective photonic bandgap control.

450 Strategically placed defects manipulate the radiation properties of the  
451 antenna whilst introducing phase shifts and altering propagation directions.  
452 Enhancing the antenna’s beam steering capabilities allows it to dynamically  
453 adjust its radiation pattern and track moving targets. Defects also mitigate  
454 losses within the substrate, enhancing radiation efficiency by minimizing scat-  
455 tering and re-absorption of electromagnetic waves. Improvement in energy  
456 transfer from the antenna to the surrounding environment improves overall  
457 performance.

### 458 3 Results and Discussion

459 The diagram of the reflection coefficient (S11) of the PhC square lat-  
460 tice is shown in Fig. 3. This antenna exhibits three resonance bands at 31.42,  
461 37.76 and 38.92 GHz covering frequency bandwidths of 1.73 GHz, 0.38 GHz  
462 and 0.78 GHz, in the ranges of [30.82, 32.55 GHz], [37.53, 37.91 GHz], and  
463 [38.40, 39.18 GHz] with a total bandwidth of 2.89 GHz. These bands are part  
464 of the  $K_a$ -band in mmWaves. The resonance bands at 31.42 GHz, 37.76 GHz  
465 and 38.92 GHz exhibit sharp dips with reflection coefficients of -17.48 dB, -  
466 24.47 dB and -41.02 dB, respectively. The antenna with square lattice includes  
467 square-shaped holes, where each side is 0.2 mm in length and the gap between  
468 adjacent holes is 0.4 mm, which contributed to its superior performance by  
469 enhancing constructive interference.

470 The S11 diagram illustrates how much electromagnetic energy is reflected  
471 back from the antenna across different frequencies. It consists of a plot show-  
472 ing the magnitude (in dB) of the reflection coefficient versus the frequency.  
473 Peaks or dips in the plot indicate the frequencies in resonance that the an-  
474 tenna is most efficient. The wider bandwidth indicates the broader frequency  
475 coverage. The diagram helps improve antenna design for efficient communi-  
476 cation.

477 The fine-tuning of the proposed antenna was achieved through improv-  
478 ing its impedance matching, demonstrating satisfactory performance across  
479 three frequency bands (31.42 GHz, 37.76 GHz), and 38.92 GHz, and provid-  
480 ing appropriate impedance matching in these ranges. As shown in Fig. 4, the  
481 values of VSWR and S11 confirm efficient power transfer and reduced signal  
482 reflection, ensuring enhanced performance.

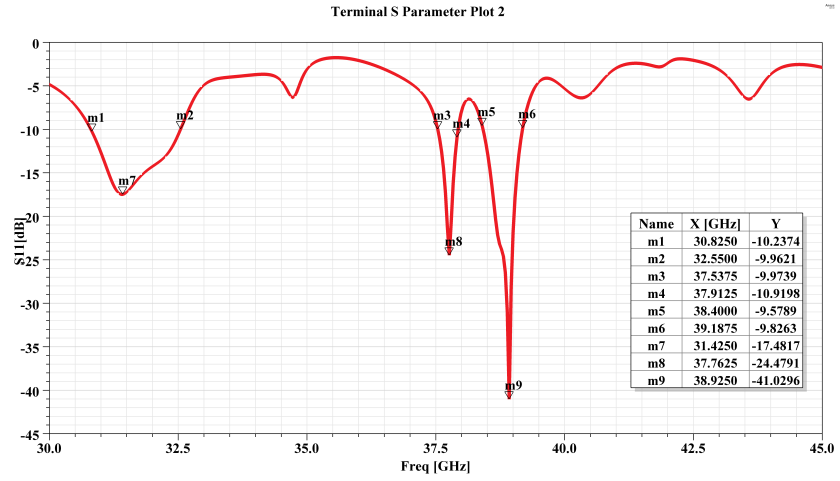


Figure 3. Reflection coefficient plot for the proposed PhC antenna with square lattice.

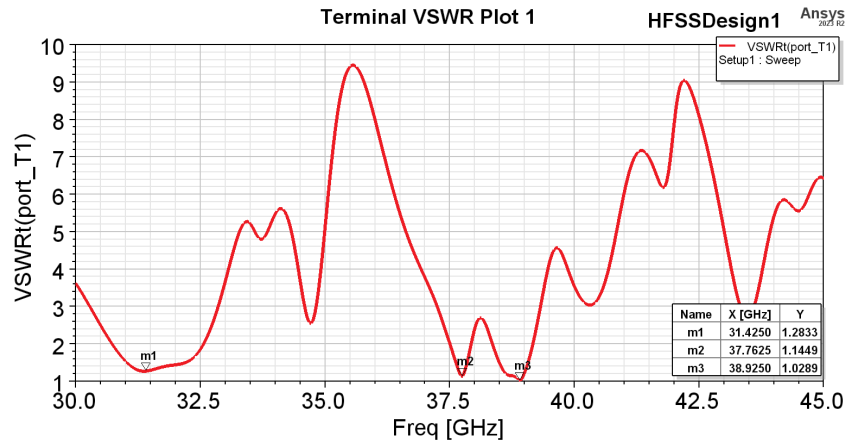


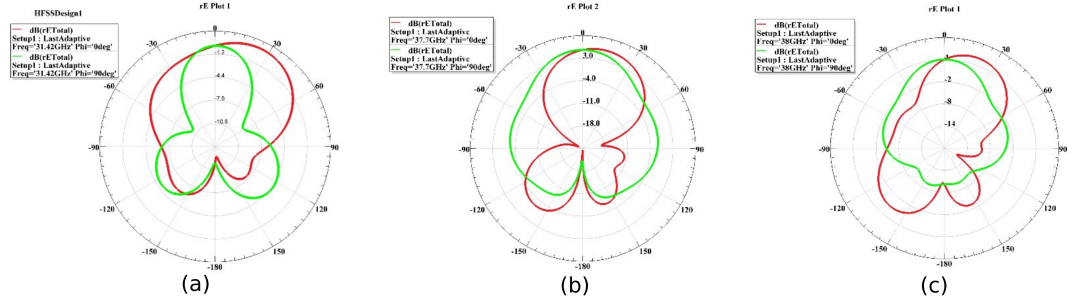
Figure 4. Plot of the VSWR for the proposed PhC antenna with square lattice.

483 In antenna design, a VSWR below 1.5 is considered excellent, while val-  
 484 ues up to 2.0 are generally acceptable for most communication applications.  
 485 Similarly, a S11 value lower than -10 dB is typically regarded as acceptable,  
 486 whereas values of -15 dB, or lower, indicate very good performance.

487 At 31.42 GHz, the VSWR is 1.28, and the S11 is -17.48 dB, indicating  
 488 appropriate impedance matching in the antenna with the square lattice. At  
 489 37.76 GHz, the VSWR is 1.14, and S11 is -24.47 dB, reflecting improved per-  
 490 formance in this band. At 38.92 GHz, the VSWR reaches 1.02, with an S11  
 491 of -41.02 dB, showing minimal reflection and maximum efficiency in this fre-  
 492 quency range. The obtained results confirm that the proposed antenna ex-  
 493 hibits stable operation across the intended frequency bands and meets the industry-  
 494 standard impedance matching requirements. The low VSWR and deep S11  
 495 values indicate excellent signal transmission with minimal return losses, mak-  
 496 ing this design highly suitable for millimeter-wave communication applica-  
 497 tions within ITS.

498 In Fig. 5 the radiation pattern plot illustrates how electromagnetic energy  
 499 is distributed in different directions from the antenna in three frequency

500 bands 31.42 GHz, 37.76 GHz and 38.92 GHz. It shows the intensity of radiation  
 501 in angular coordinates relative to the antenna's orientation. The main  
 502 lobe represents the direction of maximum radiation, whereas the side lobes  
 503 indicate the directions of secondary radiation. The plot helps to determine  
 504 the antenna's coverage area, directivity, and suitability for specific applica-  
 505 tions. The radiation pattern plot illustrates the distribution of electromag-  
 506 netic energy in various directions from the antenna, across three resonant fre-  
 507 quency bands.



**Figure 5.** Radiation pattern plot for the proposed PhC antenna with square lattice, at (a) 31.42 GHz, (b) 37.76 GHz, (c) 38.92 GHz.

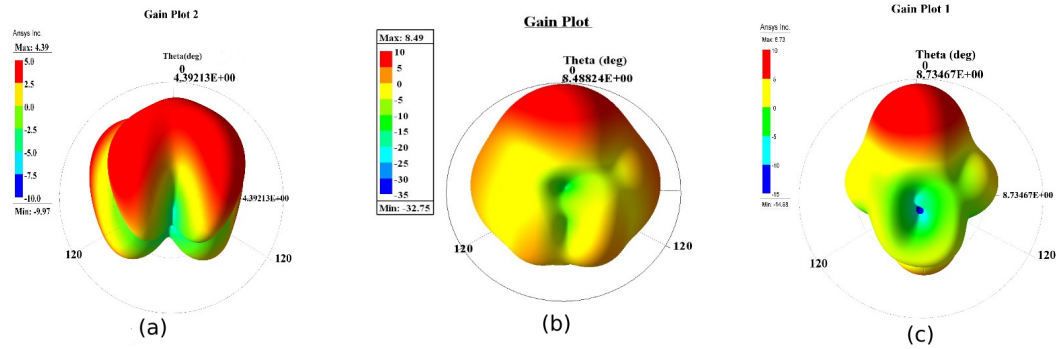
508 In Fig. 6, the gain plot shows the antenna gain characteristics in the 31.42  
 509 GHz, 37.76 GHz, 38.92 GHz frequencies. It shows the gain and directivity com-  
 510 pared to that of an ideal isotropic radiator. The gain plot provides informa-  
 511 tion on the antenna's ability to focus radiation in desired directions, aiding  
 512 in the assessment of its directional performance and efficiency. Fig. 7 which  
 513 shows the directivity plots for the proposed antenna at the three resonant fre-  
 514 quencies. These plots demonstrate the antenna's ability to effectively concen-  
 515 trate radiation in specific directions, achieving commendable directivity val-  
 516 ues of 4.34 dB at 31.42 GHz, 8.28 dB at 37.76 GHz, and 8.86 dB at 38.92 GHz.  
 517 Fig. 8 illustrates the antenna gain plot without the PhC. At 31.42 GHz, the  
 518 gain was 5.52 dB, indicating weaker impedance matching. At 37.76 GHz and  
 519 38.92 GHz, the gains were 4.58 dB and 6.15 dB, respectively, with broader  
 520 radiation patterns. In contrast, the achieved gain plot with the PhC square  
 521 lattice shown in Fig. 6, highlights a significant increase in gain resulting from  
 522 the incorporation of PhC. Inclusion of PhC not only enhances the gain of the  
 523 antenna, but also improves its directivity by enabling more focused radiation  
 524 patterns. This optimized design utilizes the PhC's properties to effectively  
 525 concentrate energy in specific directions, leading to improved signal radiation  
 526 performance and clearly demonstrate the critical role of PhC in advanced an-  
 527 tenna design, for applications that require high gain and precise directivity.  
 528 As shown in Fig. 9 by analyzing the S11 plot of the antenna without the PhC  
 529 structure, it is possible to observe a considerable decrease in bandwidth, com-  
 530 pared to the performance of the antenna that uses PhC. The antenna band-  
 531 width increases from 1.50 GHz without the photonic crystal to 2.89 GHz with  
 532 the incorporation of the photonic crystal. Fig. 10 shows the reflection coef-  
 533 ficient plot for the antenna with rectangular lattice structure. The resulting  
 534 bandwidth for this design is only 1.41 GHz, indicating moderate impedance  
 535 matching and a relatively narrower operational range. The increased band-  
 536 width in the antenna with the square lattice structure highlights its superior  
 537 performance. Showing that it is more suitable for applications that demand  
 538 both precise impedance matching and wider frequency coverage, these find-

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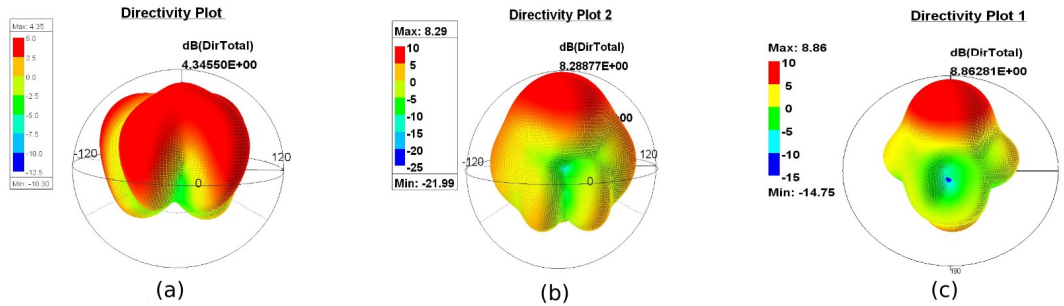
ings emphasize the role of lattice geometric in optimizing antenna bandwidth and overall efficiency for specific applications.

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At 31.42 GHz, the gains for PhC antennas with the square lattice and rectangular lattice structures are nearly identical. The square lattice PhC antenna (whose gain plots are shown in Fig. 6 (a)) demonstrates better directionality characteristics, while the rectangular lattice one exhibits a broader radiation pattern, as shown in Fig. 11 (a). At 37.76 GHz, the gain of the square lattice antenna from Fig. 6 (b) significantly outperforms the gain of the rectangular lattice antenna in Fig. 11 (b). It achieves a gain of 8.48 dB compared to 4.69 dB (for the rectangular one), with a more focused and directional radiation pattern. Similarly, at 38.92 GHz, the gain of the square lattice antenna presented in Fig. 6 (c) is higher (8.73 dB) and demonstrates superior directionality compared to the rectangular lattice antenna, whose gain is 7.06 dB (Fig. 11) (c). These results highlight the advantages of square lattice structures in terms of gain and radiation pattern.



**Figure 6.** Gain plot for the proposed PhC microstrip patch antenna with square lattice, at (a) 31.42 GHz, (b) 37.76 GHz, (c) 38.92 GHz.



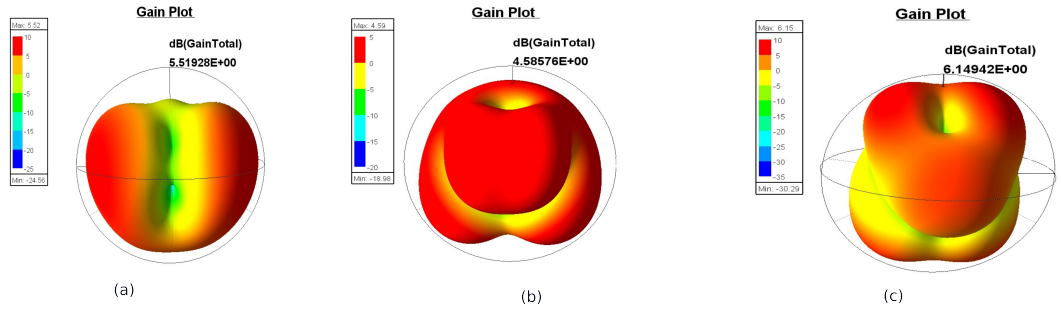
**Figure 7.** Directivity plot for the proposed PhC antenna with square lattice, at (a) 31.42 GHz, (b) 37.76 GHz, (c) 38.92 GHz.

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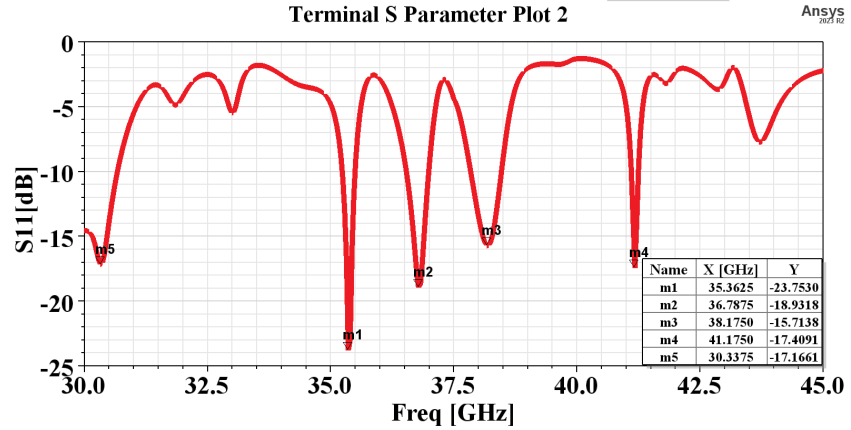
Table 1 presents a brief comparison of antenna performance metrics across different materials and frequency bands.

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It provides insights into key parameters such as gain, bandwidth, and frequency for materials such as FR-4, TLY-5, and GaAs. The tabulated data facilitate rapid assessment of each material's suitability for specific frequency



**Figure 8.** Gain of the antenna without PhC structure at (a) 31.42 GHz, (b) 37.76 GHz, (c) 38.92 GHz.



**Figure 9.** Reflection coefficient plot for the proposed antenna without PhC structure.

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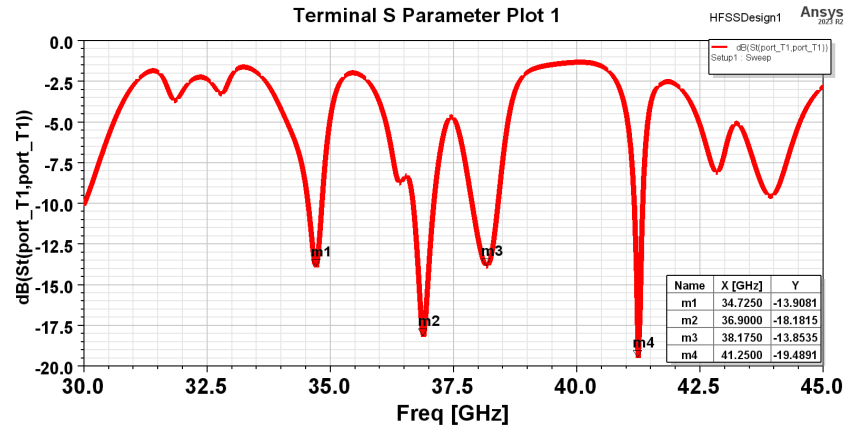
ranges, aiding in informed decision making during antenna design for various applications.

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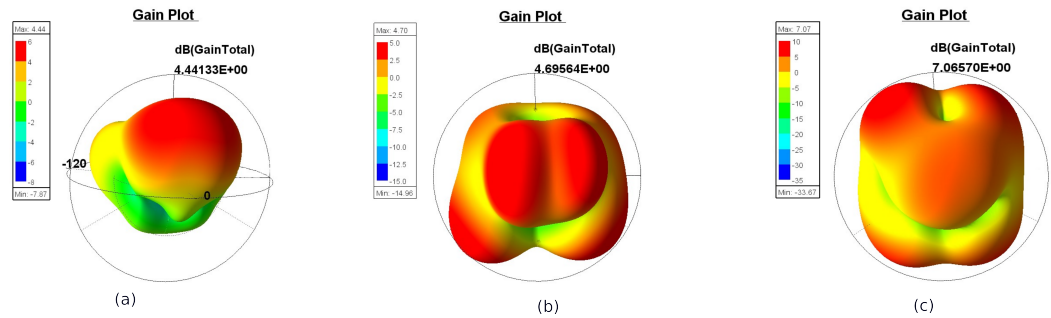
For comparison purposes, a new PhC configuration was designed by increasing the spacing between the photonic crystals and reducing the size of the square holes. Initially, the square hole side length was 0.2 mm. Then, it was reduced to 0.15 mm, while the spacing between the crystals was increased from 0.4 mm to 1.02 mm. In PhC structures, the periodicity and size of the structural features play a crucial role in determining how electromagnetic waves propagate and are guided. These changes resulted in an overall decrease in performance.

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Gain measurements indicate that at 31.42 GHz, the gain is 4.02 dB, while at 37.76 GHz, the achieved gain is 4.32 dB, showing a noticeable reduction compared to the proposed design with square lattice. Although a slight improvement was observed at 38.92 GHz, the gain increased to 6.54 dB. The structural modifications caused an increase in energy loss through radiation, disrupted constructive interference, and led to greater reflection losses. As a result, less energy was effectively transmitted, leading to weak overall performance. The gain and reflection coefficient plots for this structure are shown in Fig. 12 and Fig. 13.



**Figure 10.** Reflection coefficient plot for the proposed PhC antenna with rectangular lattice structure



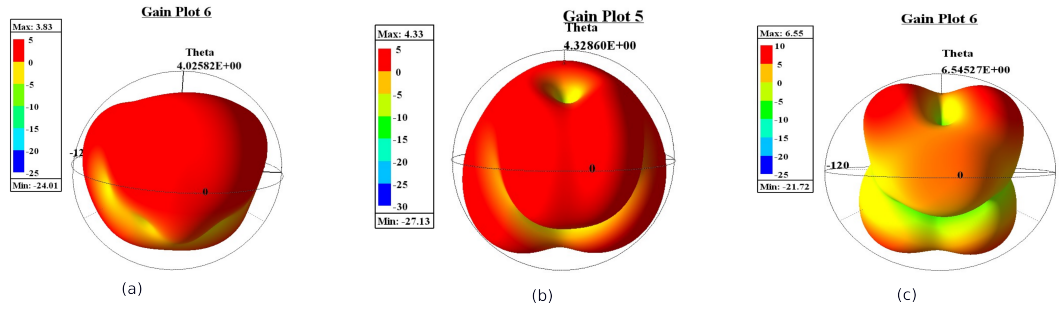
**Figure 11.** Gain plot of the proposed PhC antenna with rectangular lattice structure, at (a) 31.42 GHz, (b) 37.76 GHz, (c) 38.92 GHz.

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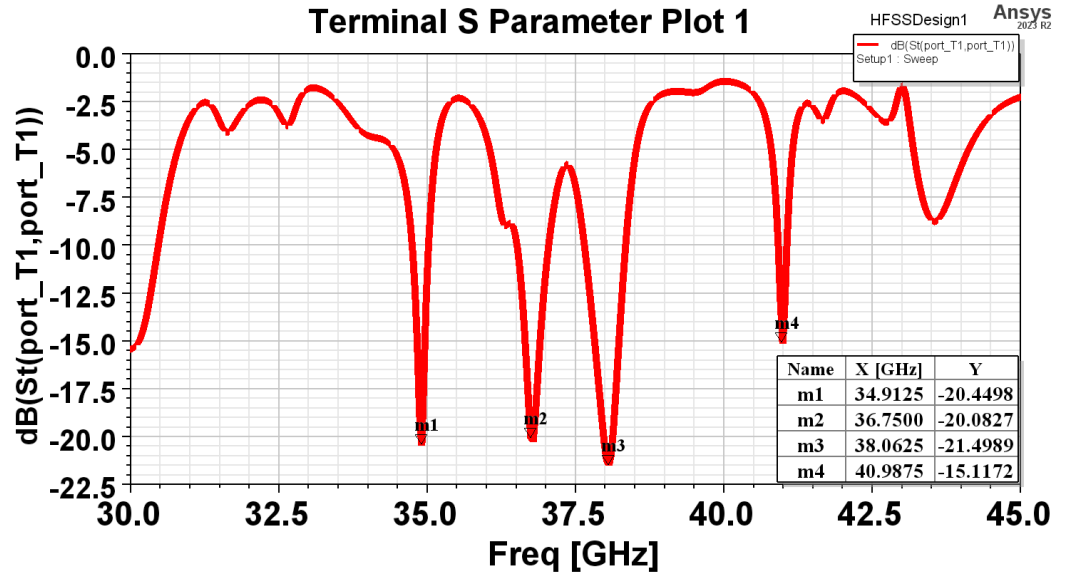
### 3.1 Phantom Model Simulations for Vehicle Mounted Antenna Analysis

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It is worthwhile to analyze the performance of the proposed antenna in realistic vehicular settings. Simulations were conducted to evaluate the performance of the proposed antenna mounted 2 mm on the rooftop of a vehicle. These simulations included a comparison of the antenna's mounted position on a car-like phantom model (whose length is 7 cm) and on a rooftop (size of 800 × 600 mm) without the car phantom model Fig. 15. Resulting 3D radiation patterns are also shown in these Figures. The simulation provides a realistic assessment of the antenna's ability to support both near-field and far-field coverage ranges. At 38.92 GHz, the gain decreases from 8.73 dB (for the proposed antenna alone) to 3.68 dB (small car) or 5.72 dB (car rooftop only). Values for the directivity are 4.00 dB and 5.81 dB for the small car and car rooftop only, respectively. Ensuring reliable signal propagation and stable field distribution in practical vehicular scenarios. These results demonstrate the antenna suitability for robust and consistent operation in real-world vehicular environments. As discussed in (Singh et al., 2017), (Imai et al., 2014), the level of detail in the phantom model significantly impacts the accuracy of the simulation results. Although a more detailed model could improve accuracy, it would also increase computational resource requirements and simulation time. These exploratory results aim to contribute and seek a balance



**Figure 12.** Gain plot of the PhC antenna with the hole side length reduced from 0.2 mm to 0.15 mm and the spacing between the crystals increased from 0.4 mm to 1.02 mm, at (a) 31.42 GHz, (b) 37.76 GHz, (c) 38.92 GHz.



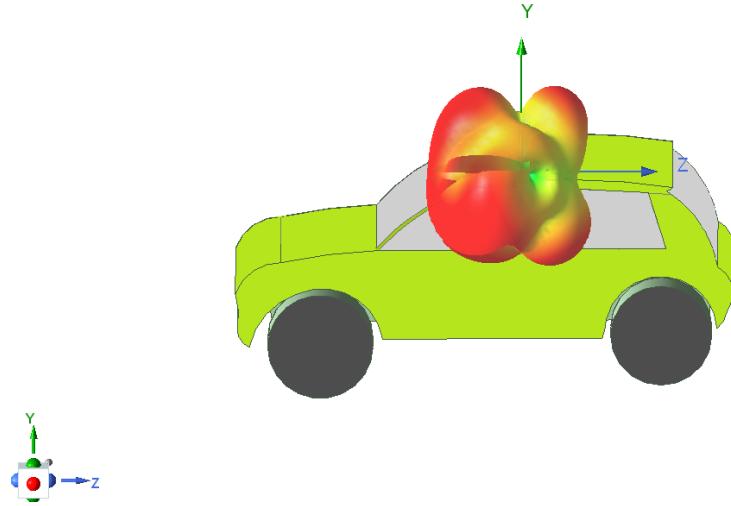
**Figure 13.** Reflection coefficient plot for the PhC antenna with the hole side length reduced from 0.2 mm to 0.15 mm and the spacing between the crystals increased from 0.4 mm to 1.02 mm.

599 between vehicle-mounted model complexity and its feasibility. Furthermore,  
 600 validation will be achieved through fabrication and experimental measurements,  
 601 which are left for future work.

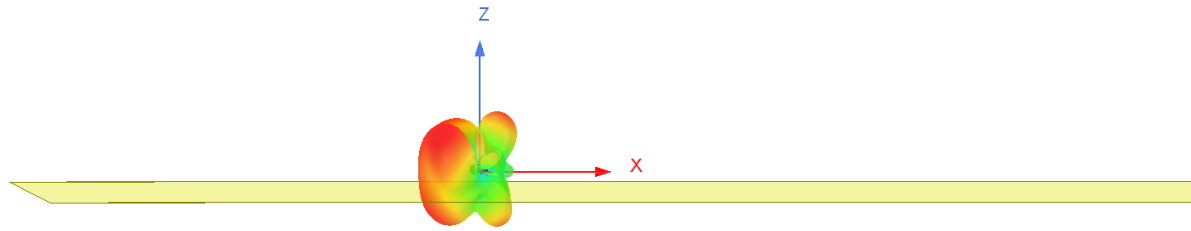
#### 602 4 Statement of Novelty

603 The paper presents an advancement in ITS through the development  
 604 of a FPA integrated with PhC for V2X communication applications on the  
 605 mmWaves. The antenna is designed to resonate at mmWaves as planned for  
 606 V2X operations.

607 One of the key characteristics of this design lies in the seamless integra-  
 608 tion of PhC within the antenna structure. By intelligently incorporating PhC  
 609 elements into the antenna substrate, the proposed design achieves enhanced  
 610 radiation efficiency and improved communication performance in mmWaves



**Figure 14.** HFSS simulation of the PhC antenna on top of car phantom model, showing the antenna's 3D radiation pattern.



**Figure 15.** HFSS simulation of the PhC antenna of on top of the car rooftop, showing the antenna's 3D radiation pattern.

611 V2X scenarios. The PhC structure acts as a PBG, effectively prohibiting spe-  
 612 cific frequencies from propagating through the substrate, thereby improving  
 613 antenna performance and mitigating undesired electromagnetic effects.

614 The bandwidth serves as a metric to determine the performance capac-  
 615 ity of an antenna or communication system. A wider bandwidth typically re-  
 616 sults in higher data transmission rates, better signal quality, and enhanced  
 617 communication capabilities.

618 Moreover, the utilization of GaAs as the substrate material is another  
 619 pivotal aspect of the design. GaAs offers properties perfectly suited for millimeter-  
 620 wave communication in V2X scenarios. Its wide bandwidth, low noise figure,

**Table 1.** Comparison of antenna performance from different studies/authors.

Material ( $\epsilon_r$ )	$f$ (GHz)	Gain(dBi)	Bandwidth (GHz)	Ref.
FR-4 (4.4)	1.50	2.14	9.70	(Kannappan et al., 2021)
	2.45	-	-	
TLY-5 (2.17-2.40)	28	7.41	1.5	(Park et al., 2016)
FR-4 (4.4)	26.5	4.93	0.3	(Mukherjee, Roy, & Mukhopadhyay, 2022)
	28	-	-	
	35	-	-	
	39	-	-	
	43	-	-	
GaAs (12.9)	31.42	6.54	1.73	(Bagheri, 2024)
	37.76	10.63	0.38	
	38.92	10.88	0.78	

**Table 2.** Performance Comparison of Different Antenna Configurations

Design Type	Frequency (GHz)	Gain (dBd)
Square Lattice	31.42	4.39
	37.76	8.48
	38.92	8.73
Without PhC	31.42	5.52
	37.76	4.58
	38.92	6.15
Rectangular Lattice	31.42	4.44
	37.76	4.69
	38.92	7.06
Square Lattice Modified Design	31.42	4.02
	37.76	4.32
	38.92	6.54

621 and high thermal conductivity contribute to the improved efficiency, reliabil-  
622 ity, and durability of the antenna system.

623 In addition, the integration of a PBG material within the GaAs substrate  
624 enables precise control over electromagnetic wave propagation, resulting in  
625 improved radiation efficiency, thus enhancing overall communication perfor-  
626 mance in ITS applications. The synergistic integration of PhC structures and  
627 GaAs substrate material represents a significant leap forward in the field of  
628 ITS communication antenna design. The approach promises to revolution-  
629 ize the ITS landscape, facilitating the foundation for more robust and efficient  
630 ITS communication networks.

## 631 5 Conclusion

632 Lately, there has been a notable trend in commercial and communica-  
633 tion systems toward the development of low-cost, lightweight, and low-profile

634 antennas capable of maintaining excellent performance across a wide frequency  
635 range. This technological shift has brought significant attention to antenna  
636 design, with a particular focus on novel configurations such as fractal nonag-  
637 onal antennas.

638 Nonagonal fractal antennas offer several benefits over traditional designs.  
639 These include low cost, compact size, ease of fabrication and installation, and  
640 compatibility with integrated circuit technology. The nonagonal fractal an-  
641 tenna proposed in this paper utilizes several advantages, including compact  
642 size, affordability, and high efficiency. With a bandwidth of 2.89 GHz and a  
643 gain of 10.88 dBi at the 38.92 GHz resonance frequency, this antenna is par-  
644 ticularly suitable for V2X applications within the FR2 frequency range. Its  
645 properties position it as a potential candidate for various communication ap-  
646 plications, including K<sub>a</sub>-band and FR2 communications, V2X communica-  
647 tions, and satellite communications.

648 Future research will involve the fabrication and testing of the designed  
649 antenna in real-world environments, after the antenna fabrication, we plan  
650 to conduct detailed measurements of the S11 response, radiation pattern, and  
651 VSWR by using an EMI/EMC testing facility.

652 Exploring the use of Barium Strontium Titanate (BST) material for the  
653 antenna substrate offers additional benefits, such as high dielectric constant  
654 and tunable permittivity, enabling miniaturization and improved performance  
655 in vehicular environments. Combining BST with photonic crystal structures  
656 enhances radiation efficiency and reduces interference while maintaining high  
657 performance for millimeter-wave V2X applications. Leveraging BST and pho-  
658 tonic crystals can achieve superior impedance matching and enhanced com-  
659 munication capabilities, contributing to the evolution of ITS. Additionally,  
660 BST's tunable properties enable dynamic adaptation to changing environmen-  
661 tal conditions, further enhancing the antenna's versatility and effectiveness  
662 in V2X.

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670 project has received funding from the European Union's Horizon 2020 research.

## 671 **Data Availability Statement**

672 This study does not involve the use of new data.

## 673 **References**

- 674 3GPP. (2021, March). *TR 38.808: Study on supporting NR from 52.6*  
675 *GHz to 71 GHz* (Tech. Spec. No. 17.0.0). 3rd Generation Partner-  
676 ship Project (3GPP).  
677 3rd Generation Partnership Project (3GPP). (2023, June). *TS 38.101-2:*  
678 *NR; User Equipment (UE) radio transmission and reception; Part*  
679 *2: Range 2 Standalone* (Tech. Spec.) Author. (Release 18, version  
680 18.2.0)

- 681 Ahangar, M. N., Ahmed, Q. Z., Khan, F. A., & Hafeez, M. (2021). A  
682 Survey of Autonomous Vehicles: Enabling Communication Tech-  
683 nologies and Challenges. *Sensors*, 21(3). Retrieved from [https://](https://www.mdpi.com/1424-8220/21/3/706)  
684 [www.mdpi.com/1424-8220/21/3/706](https://www.mdpi.com/1424-8220/21/3/706) doi: 10.3390/s21030706.
- 685 Ahmad, I., Farooque, U., & Hameed, A. (2020). Pin Loaded Triangular  
686 Patch Antenna with Embedded Spurline for Enhanced Antenna  
687 Gain. In *2020 International Youth Conference on Radio Elec-*  
688 *tronics, Electrical and Power Engineering (REEPE)* (p. 1-5). doi:  
689 10.1109/REEPE49198.2020.9059169.
- 690 Ansys. (2023). *High-Frequency Structural Simulator (HFSS)*. Retrieved 2  
691 May 2024, from [https://www.ansys.com/products/electronics/](https://www.ansys.com/products/electronics/ansys-hfss)  
692 [ansys-hfss](https://www.ansys.com/products/electronics/ansys-hfss)
- 693 Asok, A. O., & Dey, S. (2021). UWB Antipodal Antenna With Par-  
694 asitic Patch and Elliptical Cylindrical Dielectric For Concealed  
695 Object Detection with Microwave Imaging. In *2021 IEEE Inter-*  
696 *national Symposium on Antennas and Propagation and USNC-*  
697 *URSI Radio Science Meeting (APS/URSI)* (p. 741-742). doi:  
698 10.1109/APS/URSI47566.2021.9704371.
- 699 Awan, W. A., Alibakhshikenari, M., & Limiti, E. (2021). High Gain Dual  
700 Parasitic Patch Loaded Wideband Antenna for 28 GHz 5G Applica-  
701 tions. In *2021 International Symposium on Antennas and Propaga-*  
702 *tion (ISAP)* (p. 1-2). doi: 10.23919/ISAP47258.2021.9614441.
- 703 Bagheri, N. (2024). Fractal Patch Antenna based on Photonic Crys-  
704 tal for Enhanced Millimeter-Wave Communication in Intelligent  
705 Transportation Systems. *Journal Name*.
- 706 Bagheri, N., Teixeira, E., Velez, F. J., & Peha, J. M. (2024). Multi-Band  
707 Resonant Photonic Crystal Antenna for 5G Applications. In *2024*  
708 *IEEE 22nd Mediterranean Electrotechnical Conference (MELE-*  
709 *CON)* (p. 526-531). doi: 10.1109/MELECON56669.2024.10608697.
- 710 Bakir, S. S., & Sahin, A. B. (2023). Non-Destructive Defect Detection on  
711 PCB Boards Using a Metamaterial-Based Circular Patch Antenna.  
712 In *2023 Innovations in Intelligent Systems and Applications Confer-*  
713 *ence (ASYU)* (p. 1-4). doi: 10.1109/ASYU58738.2023.10296552.
- 714 Benlakehal, M. E., Hocini, A., Khedrouche, D., Temmar, M. N., Denidni,  
715 T. A., & Shayea, I. (2023, Jun 01). Design and analysis of a  $1 \times 2$   
716 microstrip patch antenna array based on photonic crystals with  
717 a graphene load in THz. *Journal of Optics*, 52(2), 483-493. doi:  
718 10.1007/s12596-022-01006-8.
- 719 Benlakehal, M. E., Hocini, A., Khedrouche, D., Temmar, M. N. e., &  
720 Denidni, T. A. (2022, Sep 13). Design and analysis of MIMO sys-  
721 tem for THz communication using terahertz patch antenna array  
722 based on photonic crystals with graphene. *Optical and Quantum*  
723 *Electronics*, 54(11), 693. doi: 10.1007/s11082-022-04081-0.
- 724 Benlakehal, M. E., Hocini, A., Khedrouche, D., Temmar, M. N. e.,  
725 Denidni, T. A., & Shayea, I. (2024, Feb 01). Design and sim-  
726 ulation of  $1 \times 2$ ,  $1 \times 4$  and  $2 \times 8$  microstrip patch antenna  
727 arrays based on photonic crystals for improved gain perfor-  
728 mance in THz. *Journal of Optics*, 53(1), 260-271. Retrieved  
729 from <https://doi.org/10.1007/s12596-023-01513-2>. doi:  
730 10.1007/s12596-023-01513-2.
- 731 Biswas, M., Ghosh, S., Mitra, C., & Gupta, B. (2023). Design and Perform-  
732 ance Analysis of Defected Grounded Hexagonal Patch Antenna at  
733 5.17 GHz. In *2023 International Conference on Computer, Electron-*  
734 *ics & Electrical Engineering & their Applications (IC2E3)* (p. 1-4).  
735 doi: 10.1109/IC2E357697.2023.10262464.

- 736 Chen, C. (2022). A Wideband Coplanar L-Probe-Fed Slot-Loaded  
737 Rectangular Filtering Microstrip Patch Antenna With High Selec-  
738 tivity. *IEEE Antennas and Wireless Propagation Letters*, 21(6),  
739 1134-1138. doi: 10.1109/LAWP.2022.3159230.
- 740 Chen, S., He, X., Zhao, R., Hu, J., & Zhang, X. (2024). Building  
741 mmWave on the evolving C-V2X: MmWave NR-V2X. *China Com-  
742 munications*, 21(1), 88-101. doi: 10.23919/JCC.fa.2023-0351.202401  
743 .
- 744 Desai, P. K., & Bindu, S. (2023). Impact of Dielectric Substrate on  
745 the performance of Microstrip Patch Antenna at millimeter wave  
746 frequency. In *2023 International Conference on Intelligent and  
747 Innovative Technologies in Computing, Electrical and Electronics  
748 (IITCEE)* (p. 629-632). doi: 10.1109/IITCEE57236.2023.10091083  
749 .
- 750 Deshmukh, R., Marathe, D., & Kulat, K. D. (2019). Microstrip Patch  
751 Antenna Gain Enhancement using Near-zero Index Metamaterial  
752 Superstrate (NZIM Lens). In *2019 10th International Conference  
753 on Computing, Communication and Networking Technologies (ICC-  
754 CNT)* (p. 1-6). doi: 10.1109/ICCCNT45670.2019.8944470.
- 755 Dong, N., Qi, N., Guo, M., Wang, C., & Chen, L. (2022). An Optimal  
756 Design of High Gain Beidou Anti-Jamming Antenna. In *2022 Inter-  
757 national Symposium on Networks, Computers and Communications  
758 (ISNCC)* (p. 1-4). doi: 10.1109/ISNCC55209.2022.9851746.
- 759 El Arrouch, T., El Amrani El Idrissi, N., & El Ansari, A. (2022). Mi-  
760 crostrip Patch Antenna using a Parasitic Mushroom for 5G Applica-  
761 tion at 28GHz. In *2022 9th International Conference on Wireless  
762 Networks and Mobile Communications (WINCOM)* (p. 1-6). doi:  
763 10.1109/WINCOM55661.2022.9966479.
- 764 Erbaş, C. D. (2020). Parametric Analysis of Angular Rotation for  
765 Microstrip Patch Antenna with Elliptical Patch and Parasitic  
766 Elements. In *2020 International Conference on Electrical, Com-  
767 munication, and Computer Engineering (ICECCE)* (p. 1-6). doi:  
768 10.1109/ICECCE49384.2020.9179237.
- 769 Fang, Y., Wu, L.-S., Qiu, L.-F., & Zhang, Y. P. (2022). A Method of  
770 Introducing Coupling Null by Shorting Pins for Stacked Microstrip  
771 Patch Antenna Array. *IEEE Transactions on Antennas and Propa-  
772 gation*, 70(7), 6030-6035. doi: 10.1109/TAP.2022.3161315.
- 773 Garcia, M. H. C., Molina-Galan, A., Boban, M., Gozalvez, J., Coll-  
774 Perales, B., Şahin, T., & Kousaridas, A. (2021). A Tutorial on  
775 5G NR V2X Communications. *IEEE Communications Surveys &  
776 Tutorials*, 23(3), 1972-2026. doi: 10.1109/COMST.2021.3057017.
- 777 Gautam, S. K., & Kumar, A. (2023). High Gain Dual-Band Shorting  
778 Pins Loaded Microstrip Patch Antenna. In *2023 IEEE Wireless An-  
779 tenna and Microwave Symposium (WAMS)* (p. 1-4). doi: 10.1109/  
780 WAMS57261.2023.10242876.
- 781 Gyawali, S., Xu, S., Qian, Y., & Hu, R. Q. (2021). Challenges and So-  
782 lutions for Cellular Based V2X Communications. *IEEE Communi-  
783 cations Surveys & Tutorials*, 23(1), 222-255. doi: 10.1109/COMST  
784 .2020.3029723.
- 785 Hakak, S., Gadekallu, T. R., Maddikunta, P. K. R., Ramu, S. P., M,  
786 P., De Alwis, C., & Liyanage, M. (2023). Autonomous vehi-  
787 cles in 5G and beyond: A survey. *Vehicular Communications*,  
788 39, 100551. Retrieved from [https://www.sciencedirect.com/  
789 science/article/pii/S2214209622000985](https://www.sciencedirect.com/science/article/pii/S2214209622000985) doi: [https://doi.org/  
790 10.1016/j.vehcom.2022.100551](https://doi.org/10.1016/j.vehcom.2022.100551).

- 791 Hamza, A., Chaabane, A., & Attia, H. (2022). Gain Improvement  
792 of Wideband Patch Antenna at Millimeter-wave Band Using  
793 Novel Metamaterial Superstrate. In *2022 16th European Con-*  
794 *ference on Antennas and Propagation (EuCAP)* (p. 1-4). doi:  
795 10.23919/EuCAP53622.2022.9769308.
- 796 Hao, S.-S., Chen, Q.-Q., Li, J.-Y., & Xie, J. (2020). A High-Gain  
797 Circularly Polarized Slotted Patch Antenna. *IEEE Anten-*  
798 *nas and Wireless Propagation Letters*, 19(6), 1022-1026. doi:  
799 10.1109/LAWP.2020.2987330.
- 800 Hossain, A. R., Nguyen, T., & Karacolak, T. (2021). A Para-  
801 sitic Patch Antenna System with High Isolation for Full Du-  
802 plex Application. In *2021 IEEE Texas Symposium on Wireless*  
803 *and Microwave Circuits and Systems (WMCS)* (p. 1-3). doi:  
804 10.1109/WMCS52222.2021.9493280.
- 805 Howell, J. (1975). Microstrip antennas. *IEEE Transactions on Antennas*  
806 *and Propagation*, 23(1), 90-93. doi: 10.1109/TAP.1975.1141009.
- 807 Imai, S., Taguchi, K., Kashiwa, T., & Kawamura, T. (2014). Effects  
808 of car body on radiation pattern of car antenna mounted on side  
809 mirror for inter-vehicle communications. In *2014 IEEE Antennas*  
810 *and Propagation Society International Symposium (APSURSI)*  
811 (p. 601-602). doi: 10.1109/APS.2014.6904631.
- 812 Jiang, H., Yan, N., Ma, K., & Wang, Y. (2023). A Wideband Cir-  
813 cularly Polarized Dielectric Patch Antenna With a Modified  
814 Air Cavity for Wi-Fi 6 and Wi-Fi 6E Applications. *IEEE An-*  
815 *tennas and Wireless Propagation Letters*, 22(1), 213-217. doi:  
816 10.1109/LAWP.2022.3201077.
- 817 K, A. S. B., & Pradeep, A. (2022). Complementary Metamaterial Su-  
818 perstrate for Wide Band High Gain Antenna. In *2022 IEEE Wire-*  
819 *less Antenna and Microwave Symposium (WAMS)* (p. 1-5). doi: 10  
820 .1109/WAMS54719.2022.9847735.
- 821 Kannappan, L., Palaniswamy, S. K., Wang, L., Kanagasabai, M., Kumar,  
822 S., Alsath, M. G. N., & Rao, T. R. (2021). Quad-Port Multiservice  
823 Diversity Antenna for Automotive Applications. *Sensors*, 21(24).  
824 Retrieved from <https://www.mdpi.com/1424-8220/21/24/8238>  
825 doi: 10.3390/s21248238.
- 826 Khabba, A., Wakrim, L., El Ouadi, Z., Amadid, J., Ibnyaich, S., & Zer-  
827 oual, A. (2022). High Gain Double U-shaped Slots Microstrip Patch  
828 Antenna Array For 28GHz 5G Applications. In *2022 International*  
829 *Conference on Decision Aid Sciences and Applications (DASA)*  
830 (p. 1589-1592). doi: 10.1109/DASA54658.2022.9765096.
- 831 Kulkarni, P. P., & Deshpande, V. S. (2024). High Gain Metamaterial  
832 Superstrate Loaded Antenna For S band Communication. In *2024*  
833 *IEEE Radio and Wireless Symposium (RWS)* (p. 140-142). doi: 10  
834 .1109/RWS56914.2024.10438511.
- 835 Kumar, D. S., Pavithra, S., Ranjith, K., Kiruthika, R., & Kavin, E.  
836 (2023). Design and Investigation of Metamaterial Antenna for  
837 Wireless Communication. In *2023 7th International Conference on*  
838 *Electronics, Communication and Aerospace Technology (ICECA)*  
839 (p. 1464-1468). doi: 10.1109/ICECA58529.2023.10395476.
- 840 Li, W., Ren, J., Zhang, B., Liu, Y.-T., Zhang, H., Yin, Y., & Shen, M.  
841 (2023). Wideband Dielectric Patch Antenna With Stable Radiation  
842 Pattern. *IEEE Antennas and Wireless Propagation Letters*, 22(7),  
843 1716-1720. doi: 10.1109/LAWP.2023.3261506.
- 844 Ligo, A. K., & Peha, J. M. (2019). Spectrum for V2X: Allocation and  
845 Sharing. *IEEE Transactions on Cognitive Communications and*

- 846                    *Networking*, 5(3), 768-779. doi: 10.1109/TCCN.2019.2916026.
- 847 Lin, H.-Y., & Omote, H. (2021). An analysis of increasing the gain  
848 of the patch antenna using slots on the ground plane. In *2020*  
849 *International Symposium on Antennas and Propagation (ISAP)*  
850 (p. 561-562). doi: 10.23919/ISAP47053.2021.9391348.
- 851 Mangal, J., & Gour, Y. (2021). A High Gain Planar Monopole Hexagonal  
852 Circular Slotted Patch Antenna For Ultra-Wideband And Multiple  
853 Frequency Range Applications. In *2021 International Conference*  
854 *on Control, Automation, Power and Signal Processing (CAPS)*  
855 (p. 1-4). doi: 10.1109/CAPS52117.2021.9730637.
- 856 Messatfa, T., Chebbara, F., & Annou, A. (2022). Analysis and De-  
857 sign of Printed Antenna Based on Photonic Crystal Substrate  
858 for 5 GHz Applications. In *2022 19th International Multi-*  
859 *Conference on Systems, Signals & Devices (SSD)* (p. 2070-2073).  
860 doi: 10.1109/SSD54932.2022.9955813.
- 861 Mishra, P., Komatineni, R., & Kulat, K. D. (2023). Millimeter Wave  
862 MPA using Metamaterial-Substrate Antenna Array for Gain En-  
863 hancement. In *2023 National Conference on Communications*  
864 *(NCC)* (p. 1-4). doi: 10.1109/NCC56989.2023.10068072.
- 865 Muangrung, B., Lang, A., Torrungrueng, D., Phongcharoenpanich, C., &  
866 Kawdungta, S. (2023). Compact High-Gain Dual-band Patch An-  
867 tenna With Dielectric Superstrate for Wi-Fi 6 Applications. In *2023*  
868 *International Electrical Engineering Congress (iEECON)* (p. 76-79).  
869 doi: 10.1109/iEECON56657.2023.10126809.
- 870 Mukherjee, K., Das, A., & Roy, S. (2020). Comparative study on a u-slot  
871 miniaturized cpw-fed multi-band antenna applicable for 5g commu-  
872 nication. In P. K. Mallick, P. Meher, A. Majumder, & S. K. Das  
873 (Eds.), *Electronic systems and intelligent computing* (pp. 707-718).  
874 Singapore: Springer Singapore.
- 875 Mukherjee, K., Mukhopadhyay, S., & Roy, S. (2022). Design of wideband  
876 planar antenna with inverted I-shaped tuning stubs for application  
877 in 5G, satellite communication, and Internet of Things. *Interna-*  
878 *tional Journal of Communication Systems*, 35. Retrieved from  
879 <https://api.semanticscholar.org/CorpusID:249680095>.
- 880 Mukherjee, K., Roy, S., & Mukhopadhyay, S. (2022). A SISO Y-  
881 Shape 5G Antenna for Intelligent Transportation Systems.  
882 In *2022 Second International Conference on Computer Sci-*  
883 *ence, Engineering and Applications (ICCSEA)* (p. 1-6). doi:  
884 10.1109/ICCSEA54677.2022.9936517.
- 885 Niranjan Prasad, J. N., Nirmal Kumar, R. G., Nirmal Kishore, A., &  
886 Jayaram, M. (2023). Tesla-geometry based wideband 5G an-  
887 tenna for V2V applications. In *2023 International Conference*  
888 *on Networking and Communications (ICNWC)* (p. 1-4). doi:  
889 10.1109/ICNWC57852.2023.10127489.
- 890 Olawoye, T. O., & Kumar, P. (2020). A High Gain Microstrip Patch  
891 Antenna with Slotted Ground Plane for Sub-6 GHz 5G Communi-  
892 cations. In *2020 International Conference on Artificial Intelligence,*  
893 *Big Data, Computing and Data Communication Systems (icABCD)*  
894 (p. 1-6). doi: 10.1109/icABCD49160.2020.9183820.
- 895 Oliveira, T. E. S., Goncalves, J. F., Reis, J. R., Vala, M., & Caldeirinha,  
896 R. F. S. (2021). High-Gain Wideband Parasitic Microstrip Antenna  
897 for 5G and IoT at 26 GHz. In *2021 Telecoms Conference (Con-*  
898 *fTELE)* (p. 1-5). doi: 10.1109/ConfTELE50222.2021.9435457.
- 899 Park, J.-S., Ko, J.-B., Kwon, H.-K., Kang, B.-S., Park, B., & Kim, D.  
900 (2016). A Tilted Combined Beam Antenna for 5G Communications

- 901 Using a 28-GHz Band. *IEEE Antennas and Wireless Propagation*  
902 *Letters*, 15, 1685-1688. doi: 10.1109/LAWP.2016.2523514.
- 903 Peha, J. M. (2023). Bringing Connected Vehicle Communications (V2X)  
904 to Shared Spectrum. In *2023 19th international conference on*  
905 *wireless and mobile computing, networking and communications*  
906 *(wimob)* (p. 431-437). doi: 10.1109/WiMob58348.2023.10187776.
- 907 Peha, J. M., Jin, Z., & de Koo, W. (2024). Vehicle-to-Everything  
908 (V2X) Communications in Unlicensed Spectrum Can Be Safe  
909 and Efficient. *IEEE Access*, 12, 181179-181191. doi: 10.1109/  
910 ACCESS.2024.3508595.
- 911 Roslan, N. H., Awang, A. H., & Hizan, H. M. (2018). The Effect of  
912 Photonic Crystal Parameters on The Terahertz Photonic Crystal  
913 Cavities Microstrip Antenna Performances. In *2018 IEEE Inter-*  
914 *national RF and Microwave Conference (RFM)* (p. 147-150). doi:  
915 10.1109/RFM.2018.8846486.
- 916 Saad, M. M., Khan, M. T. R., Shah, S. H. A., & Kim, D. (2021). Ad-  
917 vancements in Vehicular Communication Technologies: C-V2X and  
918 NR-V2X Comparison. *IEEE Communications Magazine*, 59(8),  
919 107-113. doi: 10.1109/MCOM.101.2100119.
- 920 Saad, M. M., Tariq, M. A., Seo, J., & Kim, D. (2023). An overview of  
921 3gpp release 17 & 18 advancements in the context of v2x technol-  
922 ogy. In *2023 International Conference on Artificial Intelligence*  
923 *in Information and Communication (ICAIIIC)* (p. 057-062). doi:  
924 10.1109/ICAIIIC57133.2023.10067121.
- 925 Salehi, M., Abbasian, K., & Pourziad, A. (2020). 2D-Photonic  
926 Crystal Based Bowtie Nano Antenna Designing with Spherical  
927 Gold Particles for Terahertz Applications. In *2020 28th Ira-*  
928 *nian Conference on Electrical Engineering (ICEE)* (p. 1-4). doi:  
929 10.1109/ICEE50131.2020.9261027.
- 930 Saurabh, A. K., & Meshram, M. K. (2022). Integration of Sub-6 GHz  
931 and mm-Wave Antenna for Higher-Order 5G-MIMO System. *IEEE*  
932 *Transactions on Circuits and Systems II: Express Briefs*, 69(12),  
933 4834-4838. doi: 10.1109/TCSII.2022.3197598.
- 934 Sharma, R., Raghava, N., & De, A. (2021). Design of Compact Circular  
935 Microstrip Patch Antenna using Parasitic Patch. In *2021 6th Inter-*  
936 *national Conference for Convergence in Technology (I2CT)* (p. 1-4).  
937 doi: 10.1109/I2CT51068.2021.9418104.
- 938 Singh, J., Asgharzadeh, A., Stephan, R., & Hein, M. A. (2017). Influence  
939 of Car Body Modeling on the Gain Patterns of Automotive Anten-  
940 nas. In *2017 IEEE 85th Vehicular Technology Conference (VTC*  
941 *Spring)* (p. 1-5). doi: 10.1109/VTCSpring.2017.8108214.
- 942 Sinha, P. D., Ghosh, B., & Deepa, B. (2021). Gain Enhancement of  
943 Patch Antenna Array Using a Metamaterial Superstrate. In *2021*  
944 *IEEE International Symposium on Antennas and Propagation and*  
945 *USNC-URSI Radio Science Meeting (APS/URSI)* (p. 251-252). doi:  
946 10.1109/APS/URSI47566.2021.9704344.
- 947 Soily, S., Alam, M. J., & Latif, S. I. (2022). A High Gain Cir-  
948 cularly Polarized Pin Loaded Microstrip Patch Antenna with  
949 DNG Metamaterial as Superstrate. In *2022 IEEE Interna-*  
950 *tional Symposium on Antennas and Propagation and USNC-*  
951 *URSI Radio Science Meeting (AP-S/URSI)* (p. 1454-1455). doi:  
952 10.1109/AP-S/USNC-URSI47032.2022.9887268.
- 953 Soto, I., Calderon, M., Amador, O., & Urueña, M. (2022). A survey  
954 on road safety and traffic efficiency vehicular applications based  
955 on C-V2X technologies. *Vehicular Communications*, 33, 100428.

- 956 Retrieved from [https://www.sciencedirect.com/science/](https://www.sciencedirect.com/science/article/pii/S2214209621000978)  
957 [article/pii/S2214209621000978](https://doi.org/10.1016/j.vehcom.2021.100428) doi: [https://doi.org/10.1016/](https://doi.org/10.1016/j.vehcom.2021.100428)  
958 [j.vehcom.2021.100428](https://doi.org/10.1016/j.vehcom.2021.100428).
- 959 Sufian, M. A., Hussain, N., Askari, H., Park, S. G., Shin, K. S., & Kim,  
960 N. (2021). Isolation Enhancement of a Metasurface-Based MIMO  
961 Antenna Using Slots and Shorting Pins. *IEEE Access*, 9, 73533-  
962 73543. doi: 10.1109/ACCESS.2021.3079965.
- 963 Tanveer, S., Rashid, A., & Ur-Rehman, M. (2021). A Millimeter-wave  
964 Broadband Magneto-electric Dipole Antenna Using Complementary  
965 Back Reflectors and Air-gaps. In *2021 1st International Confer-*  
966 *ence on Microwave, Antennas & Circuits (ICMAC)* (p. 1-4). doi:  
967 10.1109/ICMAC54080.2021.9678296.
- 968 Temmar, M. N., Nedil, M., & Chehri, A. (2023). Analysis and Design of  
969 Terahertz Elliptical Slot Antenna Based on Photonic Crystal Sub-  
970 strate. In *2023 IEEE International Symposium on Antennas and*  
971 *Propagation and USNC-URSI Radio Science Meeting (USNC-URSI)*  
972 (p. 197-198). doi: 10.1109/USNC-URSI52151.2023.10237916.
- 973 U.S. Department of Transportation ( October). (2024, October). *ITS*  
974 *JPO Blog: Demonstrating Interoperability for Safer Transporta-*  
975 *tion*. Retrieved from [https://www.its.dot.gov/communications/](https://www.its.dot.gov/communications/blogs/itsjpo_directors_blog_17.htm)  
976 [blogs/itsjpo\\_directors\\_blog\\_17.htm](https://www.its.dot.gov/communications/blogs/itsjpo_directors_blog_17.htm) (Accessed 2024, October)
- 977 Vahdati, A., & Parandin, F. (2019, Dec 01). Antenna Patch Design Us-  
978 ing a Photonic Crystal Substrate at a Frequency of 1.6THz. *Wire-*  
979 *less Personal Communications*, 109(4), 2213-2219. Retrieved from  
980 <https://doi.org/10.1007/s11277-019-06676-5> doi: 10.1007/  
981 s11277-019-06676-5.
- 982 Wu, D.-L., Chen, J. H., Yang, K. Y., Zhu, W. J., & Ye, L. H. (2023). A  
983 Compact Dual-Polarized Patch Antenna With L-Shaped Short Pins.  
984 *IEEE Antennas and Wireless Propagation Letters*, 22(4), 689-693.  
985 doi: 10.1109/LAWP.2022.3222338.
- 986 Yan, T.-Y., Ding, X.-H., Yang, J.-Y., & Chen, J.-X. (2024). A Low-  
987 Cost Compact Dual-Polarized Patch Antenna Array for 5G Massive  
988 MIMO Base Station. *IEEE Antennas and Wireless Propagation*  
989 *Letters*, 23(4), 1381-1385. doi: 10.1109/LAWP.2024.3356531.
- 990 Yang, Y., Zhang, X., Tan, T., Zhu, L., & Yuan, T. (2021). A Pin-Loaded  
991 and SIW-Fed Circular Patch Antenna with Stable High Gain and  
992 Wide Impedance Bandwidth. In *2021 Cross Strait Radio Science*  
993 *and Wireless Technology Conference (CSRSWTC)* (p. 304-306). doi:  
994 10.1109/CSRSWTC52801.2021.9631748.
- 995 Ye, J., Jiang, Y., & Ge, X. (2024). Deep Reinforcement Learning Assisted  
996 Hybrid Precoding for V2I Communications with Doppler Shift and  
997 Delay Spread. *IEEE Transactions on Vehicular Technology*, 1-16.  
998 doi: 10.1109/TVT.2024.3370602.
- 999 Yin, J., Chen, Z. N., Wang, H., Lou, Q., & Lai, B. (2023). Single-  
1000 Mode Dual-Band Patch Antenna Based on the Lorentz Model of  
1001 Dispersive Metamaterials. *IEEE Transactions on Antennas and*  
1002 *Propagation*, 71(11), 8580-8591. doi: 10.1109/TAP.2023.3314214.
- 1003 Zhang, D., Wang, Y., Li, X., & Xiang, W. (2018). Hybridly Connected  
1004 Structure for Hybrid Beamforming in mmWave Massive MIMO Sys-  
1005 tems. *IEEE Transactions on Communications*, 66(2), 662-674. doi:  
1006 10.1109/TCOMM.2017.2756882.
- 1007 Zhang, J., & Mao, J. (2020). A High-Gain Ka-Band Microstrip Patch  
1008 Antenna with Simple Slot Structure. In *2020 International Con-*  
1009 *ference on Microwave and Millimeter Wave Technology (ICMMT)*  
1010 (p. 1-3). doi: 10.1109/ICMMT49418.2020.9386991.

- 1011 Zhang, X., Tan, T.-Y., Wu, Q.-S., Zhu, L., Zhong, S., & Yuan, T. (2021).  
1012 Pin-Loaded Patch Antenna Fed With a Dual-Mode SIW Resonator  
1013 for Bandwidth Enhancement and Stable High Gain. *IEEE An-*  
1014 *tennas and Wireless Propagation Letters*, 20(2), 279-283. doi:  
1015 10.1109/LAWP.2020.3048749.
- 1016 Zhao, Z., Wu, L.-S., & Mao, J.-F. (2023). Ka-Band Stacked Patch  
1017 Antenna Array on Multilayer Silicon Interposer for Three-  
1018 Dimensional Integration. In *2023 International Conference on*  
1019 *Microwave and Millimeter Wave Technology (ICMMT)* (p. 1-3).  
1020 doi: 10.1109/ICMMT58241.2023.10277596.